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First Flood, unit 19, Mardon Park, Baglan Energy Park, Port Talbot, SA12 7AX T: 01639 203280

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Our ref: 21721/DSS/rca/EP/v1

Your ref:

Date: 22 August, 2024

DRAINAGE STRATEGY STATEMENT FOR PROPOSED RESIDENTIAL DEVELOPMENT AT FORMER BODLONDEB HOME, PENPARCAU, SY23 1SJ.

Roger Casey Associates has been instructed by Wales and West Housing to prepare a Drainage Strategy Statement to support a planning application for the proposed development of 18 new dwellings at the above location. The purpose of this Drainage Strategy Statement is to describe the existing drainage infrastructure and identify a sustainable solution for the proposed foul and surface water drainage serving the development, providing evidence to the Local Planning Authority that the development can be sustainably drained.

Flood Risk

The proposed use of the site, residential, will classify the risk as being a 'Highly Vulnerable Development' (TAN 15, Figure 2). However, in accordance with Natural Resources Wales Flood and Welsh Government TAN 15 Development Advice Maps¹ the site is located within an area designated being Flood Zone A.

In accordance with guidance contained within TAN 15, Figure 1, further flood risks and justification tests are not required to sites located within Zone A and sound drainage design incorporating aspects of Sustainable Urban Drainage Systems (SuDS) is applicable to the development.

Planning Policy and Technical Advice Note (TAN) 15 lists six sources of flooding which need to be considered in the assessment of flood risk and the probability of flooding at the Site Location.

Flooding from Rivers or Fluvial

Not applicable - Flood Zone A as demonstrated on Flood Map¹.

Flooding from the Sea or Tidal Flooding

Not applicable - Flood Zone A as demonstrated on Flood Map¹.

Flooding from Land

Not applicable - Flood Zone A as demonstrated on Flood Map¹.







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Flooding from Groundwater

No groundwater was struck during Quantum Geotech Site Investigations which proceeded to a depth of 3.6m below existing ground level. If groundwater is struck during further site investigations and/or construction excavations, suitable measures shall be undertaken to protect proposed and existing premises from this potential flood risk from this source.

Flooding from Sewers

Not applicable due to foul and surface water management within drainage design. Notwithstanding blockage or catastrophic failure of drainage systems within the development site resulting in overland flows not being contained within kerb upstand heights, surface gradients, etc.

Where possible, floor levels will be kept above the level of the relevant adjacent roads and drives.

Flooding from Reservoirs, Canals and Other Artificial Sources

Not applicable due to Site Location and demonstrated on Flood Map¹.

Surface Water Drainage

On 7 January 2019, the Welsh Government implemented Schedule 3 of the Flood and Water Management Act (2010). The new mandatory regulations make the incorporation of sustainable drainage systems (SuDS) compulsory in new developments exceeding 100 m² in order to help reduce flood risk and improve water quality. SuDS on new developments must be designed and built in accordance with the Statutory SuDS Standards published by the Welsh Ministers and schemes must be approved by the Local Authority acting in the role of SuDS Approving Body (SAB) before construction begins.

With reference to the Statutory Sustainable Drainage Systems Standards:

Standard S1 - Surface water runoff destination

Considering the five priority levels:

Priority Level	Flow Destination
1	Surface water run-off is collected for use;
2	Surface water runoff is infiltrated to ground;
3	Surface water runoff is discharged to a surface water body;
4	Surface water runoff is discharged to a surface water sewer, highway
	drainage, or another drainage system;
5	Surface water runoff is discharged to a combined sewer.















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Following investigations and in response to each of the Priority Levels:

- 1) Due to the development proposals, capital and long-term maintenance costs of an underground tanked rainwater harvesting system, this option is not considered as a sustainable inclusion into the surface water drainage system prior to destination. The Developer may like to consider the use of a rainwater butt with suitable overflow where appropriate.
- 2) The Quantum site investigation provides results of infiltration testing undertaken along the centre and northern edge of the side, whilst these results are favourable, when examined with the proposed levels of the development and surrounding area we deem it unsuitable to propose soakaways as a method of discharging runoff. Due to the significant drop in levels along the northern boundary infiltration features would need to be of considerable depth to avoid water travelling laterally through the existing embankment towards the dwellings of Rhyd Y Bont.
- 3) The development parcel does not benefit from a watercourse within its boundary or in the surrounding locality.
- 4) The existing building benefits from a separate surface and foul drainage systems, therefore proposals are to utilise the outfalls to the northwest of the site for the proposed development site.
- 5) This Priority Level has not been considered further due to the discharge at Priority Level 4.

Standard S2 – Surface water run-off hydraulic control

From onsite CCTV investigations no evidence of existing hydraulic control has been detected. To safequard the downstream system proposals are for the proposed development to be restricted to greenfield predevelopment runoff rate of QBar, providing a betterment when compared to the current brownfield scenario. Greenfield rates for development site have been calculated as 1.6 l/s current proposals allow for a site control hydrobrake or similar flow control device with additional smaller flow controls such as orifice plates throughout the development to maximize the attenuation to the topography where possible.

The network will be designed to accommodate all storm events up and including the 1 in 100-year event plus an allowance of 40% for climate change and 10% for urban creep.

The development proposes to utilise a number of source control methods such as permeable paving and raingardens to limit the potential for debris and litter to enter the network therefore reducing the risk of blockages and failure.

The permeable pavements beneath driveways will also act as attenuation throughout the development, with a final site control to be attenuated in the cellular storage.







Roger Casey Associates

Consulting Civil & Structural Engineers

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Standard S3 - Water quality

The proposed development will consist of several measures which have the ability to treat-run off. All parking bays are proposed to be of porous construction which will act to treat run-off at source prior to discharging into the main system.

The runoff from dwelling roofs which is deemed very low in pollutants, where suitable runoff will be directed to rain gardens and swales, which will provide treatment prior to entry into the main network.

The runoff from the adoptable highway corridor is to runoff overland towards a dished filter drain and strip along the northern boundary prior to connection to the main drainage network.

The proposals satisfy the simple index approach outlined in the CIria Suds Manual due to several features within the treatment train draining surfaces with low (driveways and residential streets) and very low levels (roofs) of pollutants.

Standard S4 – Amenity

The use of above ground SuDS measures will create a pleasant landscaping feature within the living environment whilst providing a drainage function. Permeable surfaces will create amenity of parking and access to new dwellings. SuDS measure will aim to be multifunctional. Rainwater collection will offer water for reuse for car washing, irrigation, etc.

Standard S5 – Biodiversity

The use of above ground SuDS measures such as raingardens, filter strips/drains and swale features will create linked blue/green corridors through the proposed development site. Careful landscaping and planting of these will provide a rich opportunity to maximise the biodiversity objectives of the development as a whole.

Standard S6 – Design of drainage for construction, operation and Maintenance and structural integrity

All elements of the surface water drainage system should be designed so that they can be constructed, maintenance and operation can be undertaken (by the relevant responsible body) easily, safely, cost-effectively, in a timely manner, and with the aim of minimising the use of scarce resources and embedded carbon (energy).

The surface water drainage system should be designed to ensure structural integrity of all elements under anticipated loading conditions over the design life of the development site, taking into account the requirement for reasonable levels of maintenance.













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Foul Water Drainage

A topographical survey and subsequent CCTV investigation have identified the existing routing and destination of the foul drainage routes serving the existing Bodlondeb Care Home and dwellings off Heol Y Bont.

From these investigations we understand that there is an existing 225mm combined sewer skirting the western boundary of the development whilst a separate 150mm combined sewer entering the development parcel to the rear of 1 to 5 Heol y Bont and traversers in a northerly direction towards Rhyd Y Bont. Both sewers discharge by gravity to Tan Y Cae Sewerage Pumping Station with onward conveyance to Aberystwyth (Glan Yr Avon) Sewage Works. The current development proposals respect the position of both existing combined sewers negating the requirement for sewer diversion agreements.

Onsite investigations have confirmed that the existing foul outfall of Bodlondeb Care Home is located adjacent to the vehicular access to Gwynfa and Talardd in the northwest corner of the development parcel and is proposed to being utilised as the point of connection for plots 7 to 18. This sewer communicates with the 225mm to the north of Gwynfa. Plots 1 to 6 are proposed to connect to the existing 150mm combined sewer located to their rear.

Where the new foul water drainage system lies outside of the legal curtilage of the proposed plots it will need to be adopted by Dwr Cymru Welsh Water under a Water Industry Act Section 104 Adoption Agreement between DCWW and the Developer.

Connection to the public sewer will be subject to a Water Industry Act 1991 Section 106 application and will take the form of either alteration to an existing chamber or construction of a new chamber on the line of the existing sewer.













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Summary

This Drainage Strategy Statement concludes that an achievable and sustainable drainage scheme can be designed for both foul and surface water drainage systems:

- All proposed development works are located in a low flood risk location considered by TAN 15.
- Surface water flows drained by gravity to onsite surface water drain via suitable SuDS measures and attenuated to greenfield (preexisting development) runoff rate of 1.6l/s.
- Foul water flows drained by gravity to the existing public foul water sewer network on site.

Edward Powell MEng GMICE Civil Engineer e.powell@rca-eng.co.uk

for Roger Casey Associates

Encs:

- ¹ National Resources Wales Flood Risk Map and Welsh Government TAN 15 Development Advice
- ² Soakaway Extracts from Quantum Geotech Phase II: Ground Investigation Interpretative Report dated August 2023
- ³Concept Drainage Strategy Plan

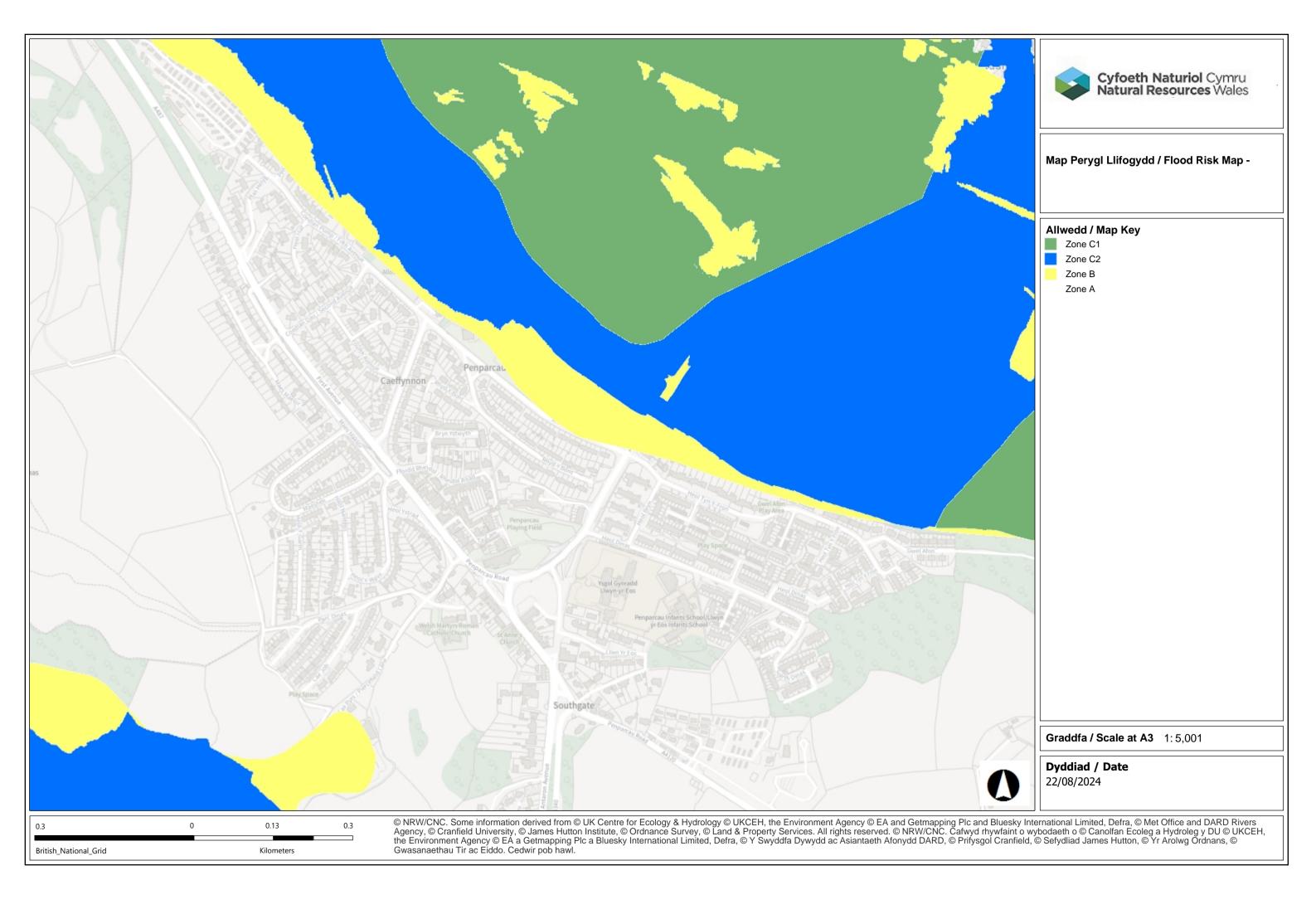


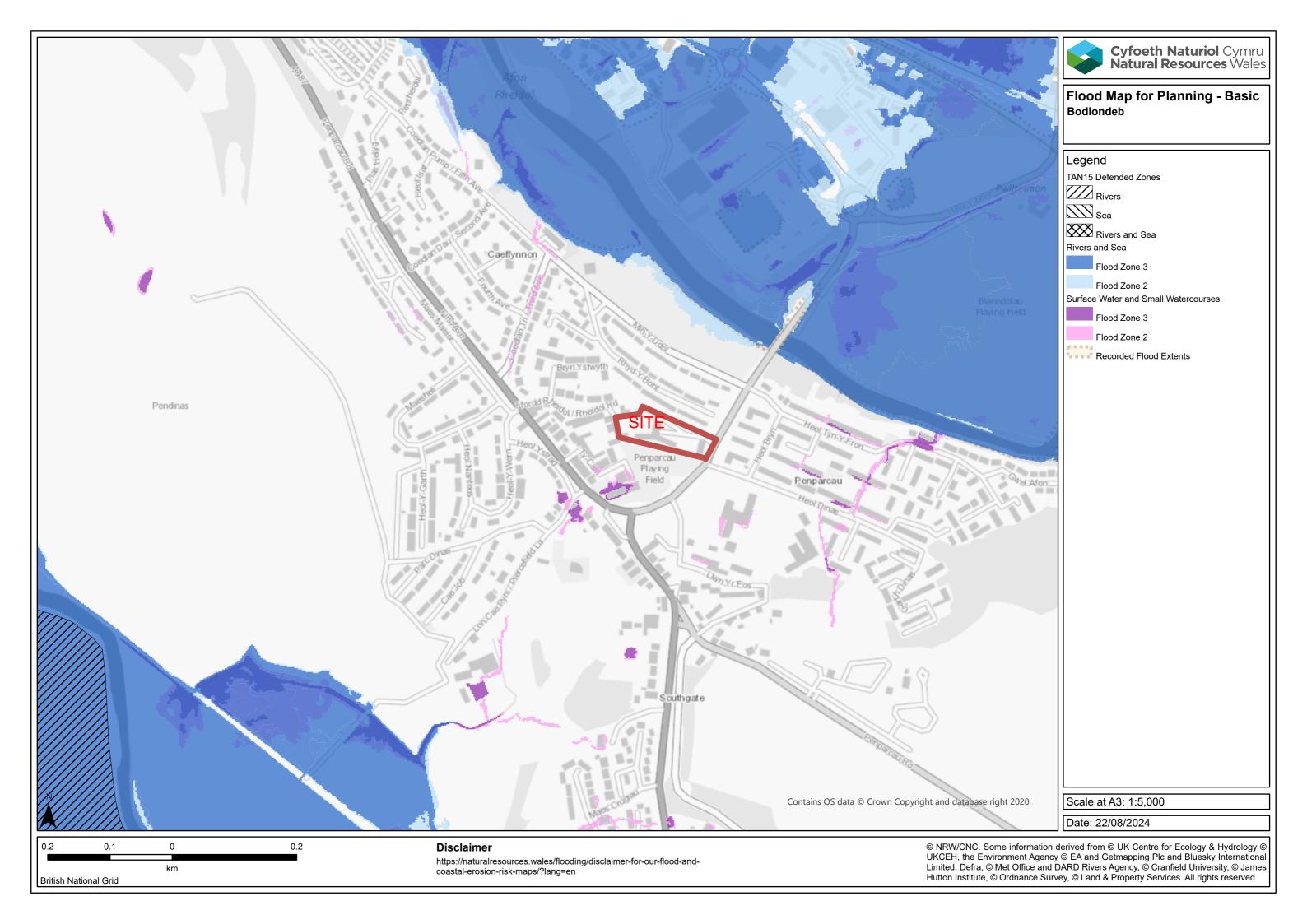














5.0 GROUND CONDITIONS ENCOUNTERED

5.1 General

The sequence of deposits encountered during the investigation is detailed within the Engineering Geologist's logs presented within Appendix II and III. The following sections summarise the findings of the exploratory holes.

5.2 Ground Conditions

5.2.1 Overview of Strata Encountered

The ground conditions encountered across the site generally comprised a surface layer of Topsoil or Tarmac. Made Ground was encountered below the Topsoil / Tarmac within the exploratory holes undertaken to the north of the main nursing home building. Underlying the Made Ground, or directly below the Topsoil within the exploratory holes to the south of the building, either Head Deposits or weak / weathered Siltstone (Aberystwyth Grits Formation) were encountered. Where no Head Deposits were present, the Topsoil / Tarmac was directly above weathered and / or weak Siltstone (Aberystwyth Grits Formation). A summary of the ground conditions encountered is presented in Table 8.

Conoral Strata Description	Elevation of base of Strata (mbgl)									
General Strata Description	TP1	TP2	TP3	TP4	TP5	TP6	ТР7	TP8		
Topsoil	0.08	0.07	0.07	0.06		0.05	0.06			
Tarmac								0.08		
Made Ground		0.8	1.8	0.9	0.35	1.05		0.3		
Head Deposits		1.4	2.3		0.8		0.8	2.2+		
Aberystwyth Grits Formation	2.0+	2.0+	3.0+	1.4+	3.0+	3.0+	2.0+			
	WS1	WS2	WS3	WS4	WS5	WS6	WS7	WS8	WS9	WS10
Topsoil			0.1	0.1	0.1		0.1			
Tarmac	0.07	0.07						0.25	0.25	0.25
Made Ground	0.4					0.5		1.6		
Head Deposits			0.9		1.5			1.9		
Aberystwyth Grits Formation	2.0+	0.9+	1.7+	0.7+	2.7+	1.9+	0.8+	3.6+	1.4+	1.4+

⁻⁻ Strata not encountered within exploratory hole

Topsoil / Tarmac

Topsoil was encountered within all the exploratory holes undertaken within the grassed areas of the site to depths of between 0.05 and 0.1mbgl.

⁺ Depth of strata not proven



A layer of Tarmac was encountered within all exploratory holes undertaken within the areas of hardstanding, to depths of between 0.07 and 0.25mbgl.

Made Ground

Made Ground was encountered within the majority of exploratory holes undertaken to the north of the nursing home building. The Made Ground generally comprised brown clayey slightly silty slightly sandy siltstone, brick, tile and glass Gravel with brick cobble content, and grey slightly silty slightly sandy siltstone, sandstone and brick Gravel. The Made Ground was proven to depths of between 0.3 and 1.8mbgl.

Head Deposits

Pockets of soil interpreted to be Head Deposits were encountered either underlying the Made Ground or directly below the Topsoil where Made Ground was not found to be present. These deposits were encountered to depths of between 0.8 and 2.3mbgl.

Aberystwyth Grit Formation

Within each exploratory hole, with the exception of TP8, strata interpreted to be the Aberystwyth Grit Formation was encountered either below the Made Ground deposits or the Head Deposits. These deposits were either highly weathered to slightly silty sandy Gravel or weak Siltstone. The competency of these deposits increased with depth and the exploratory holes terminated upon refusal at depths of between 0.7 and 3.0mbgl.

5.2.2 Groundwater Conditions

No groundwater was encountered during the investigation or post fieldwork monitoring.

Please Note: The groundwater conditions observed in these exploratory holes are those appertaining to the period of the investigation and monitoring. However, it should be noted that groundwater levels are subject to diurnal, seasonal and climatic conditions or may vary due to other causes.

5.2.3 Visual & Olfactory Evidence of Soil Contamination

No visual or olfactory evidence of soil contamination was observed/ recorded.

5.2.4 Visual & Olfactory Evidence of Groundwater & Surface Water Contamination

No visual or olfactory evidence of any groundwater contamination or surface water contamination during the investigation works was observed/ recorded.



APPENDIX IV - SOAKAWAY TEST CERTIFICATES

Client: Wales and West Housing

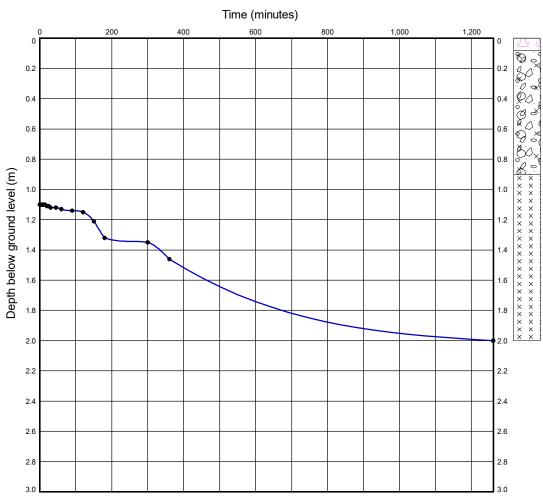
Job Number: Q1149 Engineer: Roger Casey Associates

Point Plotted TP1,1

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit





Remarks:

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 2.000 m V_{p75-25} = 0.450 m³ Trial Pit Length 2.500 m a_{p50} = 3.485 m²

Trial Pit Width 0.800 m t_{p75-25} = 450.000 minutes

Effective Depth 0.450 m

Outflow Time 450 mins from 75% to 25% full

f = 4.7824E-6 m/sec



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Date of Test: 14/06/2023

Project File: Q1149.GPJ

All measurements in metres unless otherwise stated

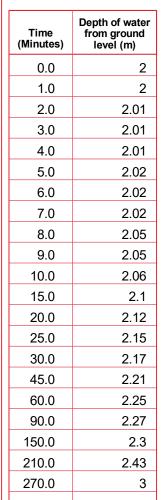
Client: Wales and West Housing

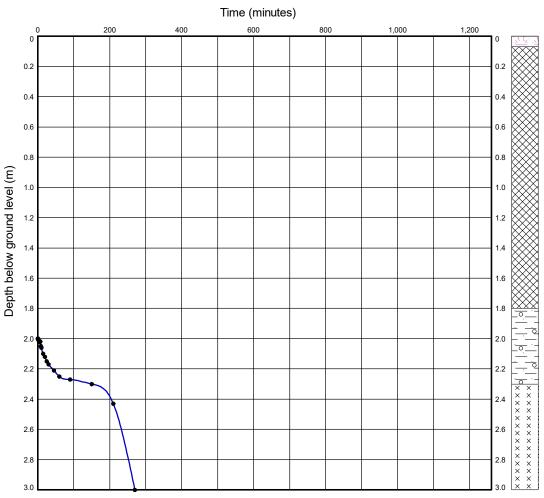
Job Number: Q1149 Engineer: Roger Casey Associates

Point Plotted TP3,1

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit





Remarks:

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 3.000 m V_{p75-25} = 0.500 m³ Trial Pit Length 2.500 m a_{p50} = 3.650 m²

Trial Pit Width 0.800 m t_{p75-25} = 190.000 minutes

Effective Depth 0.500 m

Outflow Time 190 mins from 75% to 25% full

f = 1.2016E-5 m/sec



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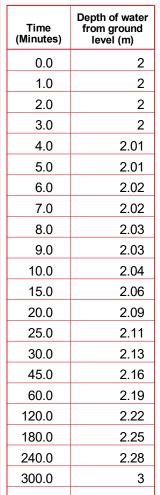
Client: Wales and West Housing

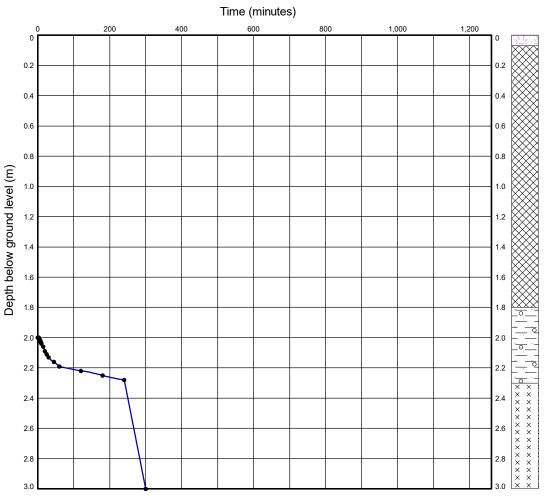
Job Number: Q1149 Engineer: Roger Casey Associates

Point Plotted TP3,2

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit





Remarks:

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 3.000 m V_{p75-25} = 0.500 m³ Trial Pit Length 2.500 m a_{p50} = 3.650 m²

Trial Pit Width 0.800 m t_{p75-25} = 100.000 minutes

Effective Depth 0.500 m

Outflow Time 100 mins from 75% to 25% full

f = 2.2831E-5 m/sec



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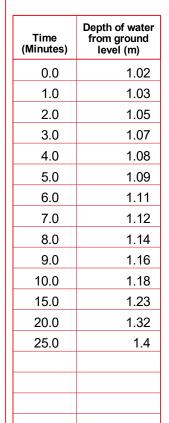
Client: Wales and West Housing

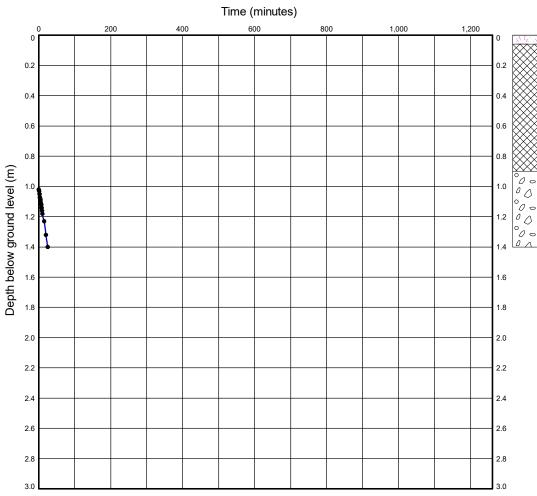
Job Number: Q1149 Engineer: Roger Casey Associates

Point Plotted TP4,1

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit





Remarks:

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 1.400 m V_{p75-25} = 0.200 m³ Trial Pit Length 2.500 m a_{p50} = 2.660 m²

Trial Pit Width 0.800 m t_{p75-25} = 14.000 minutes

Effective Depth 0.200 m

Outflow Time 14 mins from 75% to 25% full

f = 8.9509E-5 m/sec



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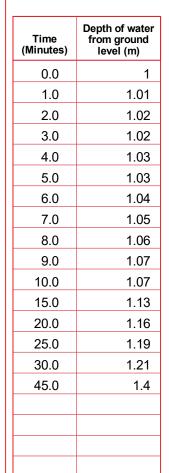
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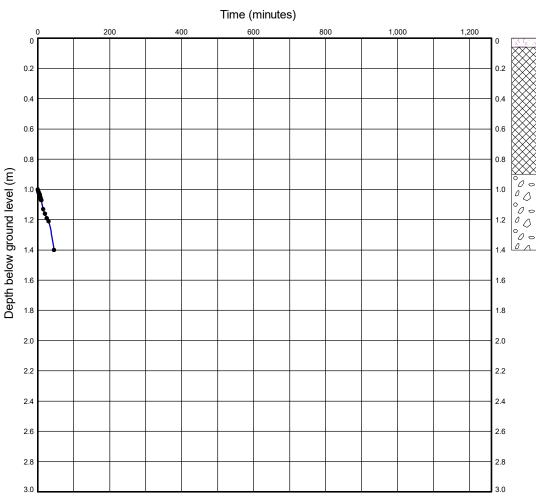
Job Number: Q1149 Engineer: Roger Casey Associates

Point Plotted TP4,2

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit





Remarks:

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 1.400 m V_{p75-25} = 0.200 m³ Trial Pit Length 2.500 m a_{p50} = 2.660 m²

Trial Pit Width 0.800 m t_{p75-25} = 26.000 minutes

Effective Depth 0.200 m

Outflow Time 26 mins from 75% to 25% full

f = 4.8197E-5 m/sec



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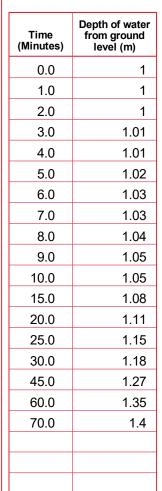
Client: Wales and West Housing

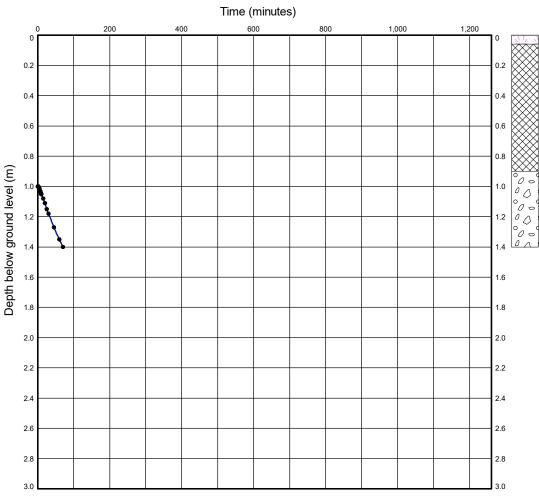
Job Number: Q1149 Engineer: Roger Casey Associates

Point Plotted TP4,3

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit





Remarks:

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 1.400 m V_{p75-25} = 0.200 m³ Trial Pit Length 2.500 m a_{p50} = 2.660 m²

Trial Pit Width 0.800 m t_{p75-25} = 30.000 minutes

Effective Depth 0.200 m

Outflow Time 30 mins from 75% to 25% full

f = 4.1771E-5 m/sec



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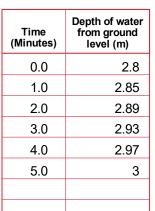
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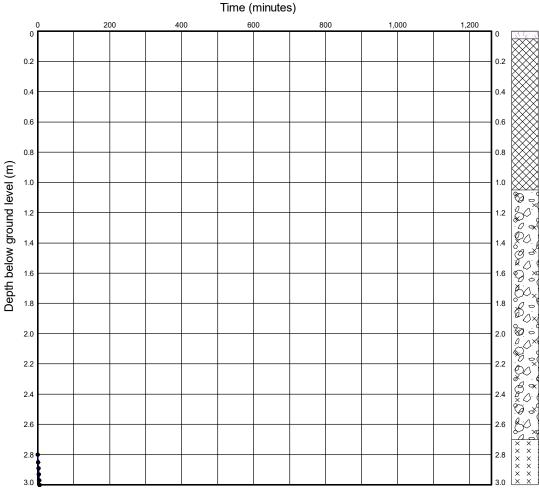
Job Number: Q1149 Engineer: Roger Casey Associates

Point Plotted TP6,1

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit





Remarks: Unable to raise head of water - 1000l pumped into hole

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 3.000 m V_{p75-25} = 0.100 m³ Trial Pit Length 2.500 m a_{p50} = 2.330 m²

Trial Pit Width 0.800 m t_{p75-25} = 2.000 minutes

Effective Depth 0.100 m

Outflow Time 2 mins from 75% to 25% full

f = 3.5765E-4 m/sec



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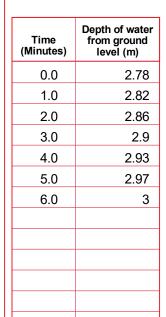
All measurements in metres unless otherwise stated

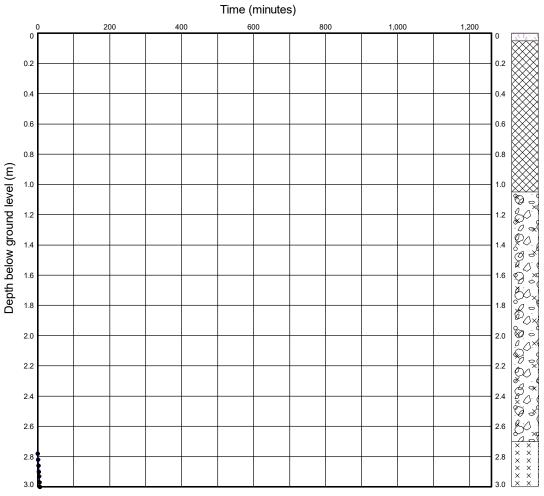
Client: Wales and West Housing

Job Number: Q1149 Engineer: Roger Casey Associates

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit





Remarks: Unable to raise head of water - 1000l pumped into hole

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 3.000 m V_{p75-25} = 0.100 m³ Trial Pit Length 2.500 m a_{p50} = 2.330 m²

Trial Pit Width 0.800 m t_{p75-25} = 2.000 minutes

Effective Depth 0.100 m

Outflow Time 2 mins from 75% to 25% full

f = 3.5765E-4 m/sec



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Point Plotted

TP6,2

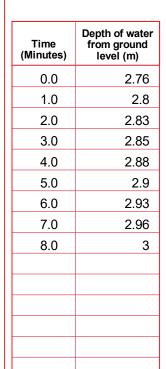
Client: Wales and West Housing

Q1149

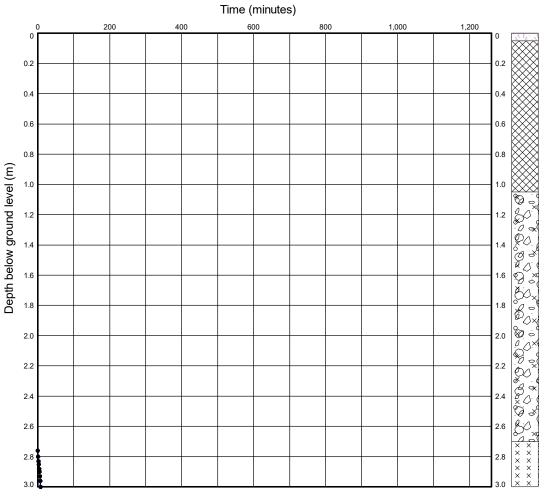
Engineer: Roger Casey Associates

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit



Job Number:



Remarks: Unable to raise head of water - 1000l pumped into hole

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 3.000 m V_{p75-25} = 0.110 m³ Trial Pit Length 2.500 m a_{p50} = 2.363 m²

Trial Pit Width 0.800 m t_{p75-25} = 2.000 minutes

Effective Depth 0.110 m

Outflow Time 2 mins from 75% to 25% full

f = 3.8792E-4 m/sec



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Point Plotted

TP6,3

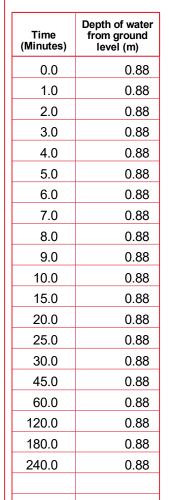
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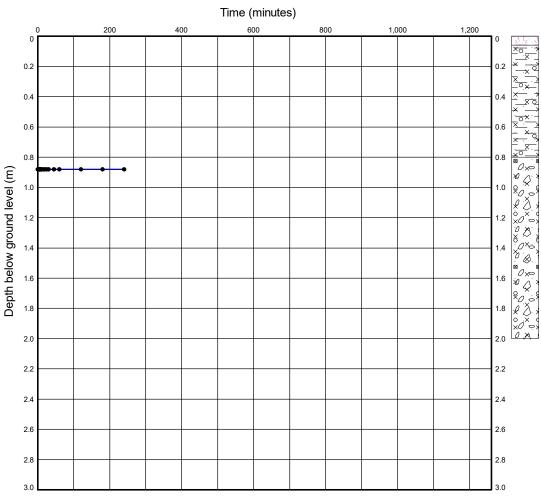
Job Number: Q1149 Engineer: Roger Casey Associates

Point Plotted TP7,1

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit





Remarks: Insufficient outflow to calculate permeability.

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 2.000 m V_{p75-25} = m^3 Trial Pit Length 2.500 m a_{p50} = m^2

Trial Pit Width 0.800 m t_{p75-25} = minutes

Effective Depth m

Outflow Time mins from 75% to 25% full

f = m/sec



Plas Newydd Swansea Tel: 01554744880 Tel: email: enquiries@quantumgeotechnic.co.uk

Date of Test: 15/06/2023

Project File: Q1149.GPJ

All measurements in metres unless otherwise stated

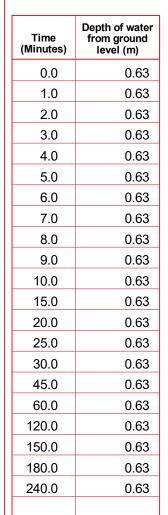
Client: Wales and West Housing

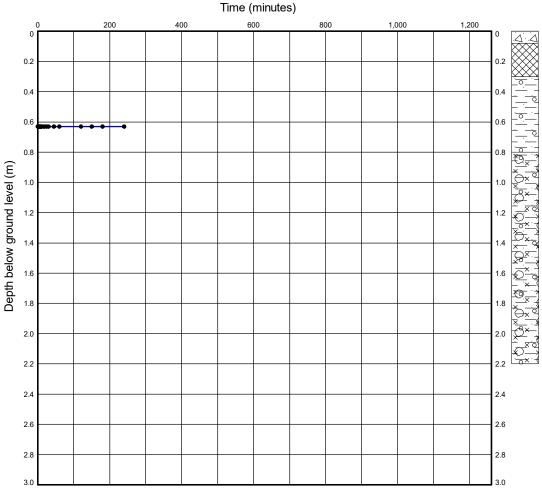
Job Number: Q1149 Engineer: Roger Casey Associates

Point Plotted TP8,1

SOAKAWAY TEST CALCULATION SHEET

Field Observations from soakaway trial pit





Remarks: Insufficient outflow to calculate permeability

Soakaway test for soil infiltration rate design method based on BRE Digest 365

Permeability Test on Strata

Trial Pit Depth 2.200 m V_{p75-25} = m^3 Trial Pit Length 2.500 m a_{p50} = m^2

Trial Pit Width 0.800 m t_{p75-25} = minutes

Effective Depth m

Outflow Time mins from 75% to 25% full

f = m/sec



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